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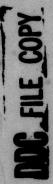
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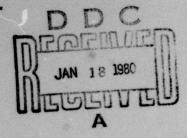
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OF THE PE PLE ONE DIMENSIONAL MODELS OF THE PENETRATION OF RODS

Robert E. LoLovier





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SIMPLE ONE DIMENSIONAL MODELS OF THE PENETRATION OF RODS

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December 1979

SECURITY CLASSIFICATION OF THIS PAGE (When Date Enter READ INSTRUCTIONS BEFORE COMPLETING FORM REPORT DOCUMENTATION PAGE RESORT NUMBER 2. GOVT ACCESSION NO. 3. RECIPIENT'S CATALOG NUMBER SRI-JSN-79-09 TITLE (and Subtitle) S. TYPE OF REPORT & PERIOD COVERED Technical Note Simple One Dimensional Models of the Penetration of Rods, 6. PERFORMING ORG. REPORT NUMBER JSN-79-09 V 7. AUTHOR(s) B. CONTRACT OR GRANT NUMBER(s) Robert E./LeLevier MDA903-78-C-0086 DODARPA Order - 2509 9. PERFORMING ORGANIZATION NAME AND ADDRESS AREA & WORK UNIT NUMBERS SRI International V 1611 N. Kent Street A.O. 2504, 27 & 28 Arlington, VA 22209 12. REPORT DATE 13. NO. OF PAGES 11. CONTROLLING OFFICE NAME AND ADDRESS 79 Dec Advanced Research Projects Agency 15. SECURITY CLASS. (of this report) 1400 Wilson Boulevard Arlington, VA 22209 UNCLASSIFIED 14. MONITORING AGENCY NAME & ADDRESS (if diff. from Controlling Office) 150. DECLASSIFICATION / DOWNGRADING 16. DISTRIBUTION STATEMENT (of this report) Cleared for open publication; distribution unlimited. 17. DISTRIBUTION STATEMENT (disclaimer) The views and conclusions contained in this document are those of the author and should not be interpreted as necessarily representing the official policies, either expressed or implied, of the Advanced Research Projects Agency or of the U.S. Government. 18. SUPPLEMENTARY NOTES 19. KEY WORDS (Continue on reverse side if necessary and identify by block number) ARMOR PENETRATION LONG ROD PENTRATORS 20. ABST/MACT (Continue on reverse side if necessary and identify by block number) This note discusses a simple one dimensional model for describing the penetration of armor by rods based upon work by Alekseevshii and Gogolewski. We show that these models give incorrect results because they assume that the mass of the target material is constant, not a function of time as it actually is. We show that assuming this time dependence of the mass, yields results quite consistent with experimental data.

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## SDIPLE ONE DEMENSIONAL MODELS OF THE PENETRATION OF RODS

There are a large number of simple, one-dimensional models which attempt to provide estimates of the penetration of rods in target materials. Some of the models become quite sophisticated. For example, the ARAP work attempts to include the effects of target heating in the flow about the intruding projectile.

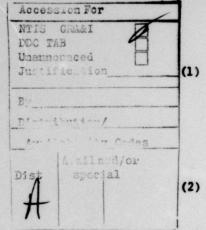
Ray Gogolewski, TTO, DARPA, discussed a particularly simple model which purported to agree essentially with the data and which provided useful scaling laws. This model is based on Alekseevshii's work [1] and introduces the concept of mass erosion of the penetrator where u is the erosion speed in the target and is related to w, the speed of the projectile by,

$$u = \frac{w}{1+f} \quad ,$$

where the parameter f is given by

$$f = \left(\frac{\rho_t}{\rho_p}\right)^{1/2} .$$

0



In Equation (2),  $\rho_t$  is the target density and  $\rho_p$  , that of the penetrator.

Gogolewski's model begins with the conservation of momentum written as,

$$\mathbf{n} \frac{d\mathbf{v}}{dt} = -\sigma_{\mathbf{p}} \mathbf{A} \quad , \tag{3}$$

Where  $\sigma_{p}$  is the yield stress of the rod, A the cross sectional area and m the mass which is decreasing with time due to erosion. This cannot be the correct momentum equation because the mass is varying with time. In the spirit of these simple models the momentum equation should read,

$$\frac{d}{dt} = -\sigma_{\rho} A \qquad (4)$$

Let us discuss this more correct model and return to the Gogolewski approach, Eq. (3), later on-

Equation (4) is immediately integrated to give,

$$\mathbf{m} = \mathbf{n}_0 \mathbf{v}_0 \left(1 - \frac{\mathbf{t}}{\mathbf{t}}\right) \qquad , \tag{5}$$

where  $m_0$  and  $w_0$  are the initial mass and speed of the penetrator and the time constant  $\tau$  is,

$$\tau = \frac{\mathbf{w}_0 \ \mathbf{w}_0}{\sigma_0 \mathbf{A}} \quad . \tag{6}$$

The rate of mass erosion is,

i.

x

$$\frac{d\mathbf{n}}{dt} = \mathbf{A} \rho_{\mathbf{p}} \quad (\mathbf{w} - \mathbf{u})$$

$$= -A \rho_{p} \frac{f}{1+f} w \qquad . \tag{7}$$

Eq. (7) can be integrated with the help of Eq. (5) to give,

$$m^2 = m_0^2 \left[1 - k\chi \left(1 - \frac{\chi}{2}\right)\right]$$
, (8)

where  $\chi = t/\tau$  and the constant k is,

$$k = 2 \rho_{p} \frac{f}{1+f} \frac{w_{o}^{2}}{\sigma_{p}} . \qquad (9)$$

The penetration P is given by

$$P = \int_{0}^{t} u dt \qquad . \tag{10}$$

Performing this integral we get,

$$P = L \sqrt{\frac{\rho_p}{\rho_t}} \left\{ 1 - \sqrt{1 - \frac{f}{1+f}} \rho_p \frac{w_o^2}{\sigma_p} \right\} , \qquad (11)$$

where L is the original length of the penetrator.

This expression for penetration leads to the result,

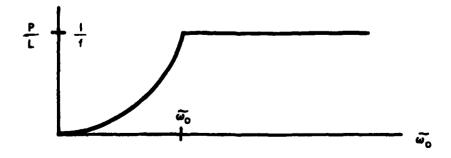
$$P = \frac{L}{2} \frac{\rho_p}{l+f} \frac{w_o^2}{\sigma_p} , \quad w_o^2 \ll \frac{\sigma_p}{\rho_p} , \qquad (12)$$

or the penetration depth is proportional to the initial kinetic energy of the rod. This agrees with experiments in the speed domain indicated.

For very large initial speeds the mass erodes to zero before the speed of the rod goes to zero. Consequently, the penetration approaches the value,

$$P = L \sqrt{\frac{\rho_p}{\rho_t}} , \quad w_o^2 >> \frac{\sigma_p}{\rho_p} . \qquad (13)$$

This also seems to be a well known limit which agrees with experiments in the indicated speed domain. Thus we expect the penetration as a function of initial speed to look like,



in agreement with the data presented.

The crossover speed  $w_0^2$  is given by,

$$w_{o} = \left(\frac{1+f}{f} \quad \frac{\sigma_{p}}{P_{p}}\right)^{1/2} \tag{14}$$

Eqs. (11), (12) and (13) give about as much information on scaling as one can reasonably expect from such a simple one-dimensional model.

Turning to the other momentum equation (Eq. (3)), one can show that the speed w is related to the time t by,

$$\exp\left(\frac{w_o^2}{2c_o^2}\right)_w^{W_o} \exp\left(\frac{w^2}{2c_o^2}\right) dw = \frac{\sigma_p A t}{m_o}, \qquad (15)$$

where

$$c_0^2 = \frac{1+f}{f} \frac{\sigma_p}{\rho_p} . \tag{16}$$

Again, if  $\frac{w^2}{2c_0^2} \ll 1$  we find,

$$P = \frac{1}{2} L \frac{\rho_p}{1+f} \frac{v_o^2}{\sigma_p} , \qquad (17)$$

as before. On the other hand, as  $w_0$  increases, the penetration increases without bound which seems to contradict the data!

## LIST OF REFERENCES

V. P. Alekseevshii, "Penetration of a Rod into a Target at High Velocity", Fizika Goreniya i Vzvyva, Vol. II, #2, p. 99-106, (1966), UDC532.501.32

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